

SPECIFICATION

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT I, KEN KANAI, a citizen of Japan residing at Tokyo, Japan have invented certain new and useful improvements in

METHOD FOR REDUCING ELECTROMAGNETIC DISTURBANCE WAVE
AND HOUSING STRUCTURE

of which the following is a specification:-

BACKGROUND OF THE INVENTION

1. Field of the Invention

The present invention relates to methods for reducing electromagnetic disturbance waves and housing structures, the electromagnetic disturbance being generated at the housings having electronic apparatuses.

2. Description of the Related Art

Recently, although various kinds of apparatuses where an electric apparatus is installed have become widespread, electromagnetic waves generated from the electric apparatuses is a problem under a recent trend where the electric apparatus has a high quality function of and a high clock speed. Particularly, in an image reader part of an image forming machine such as a copy machine, the clock frequency becomes high for accomplishment of high quality output. Because of this, influence of leakage of electromagnetic wave noises on various parts become a more serious problem.

There is a related art copy machine having a housing structure similar to the present invention, as described in the Japanese Laid-Open Patent Application, H05-199340. This related art copy machine has a structure, wherein an electronic

apparatus section, having electronic parts such as an image read part, an image write part, and a primary signal processing part for corrective processing of an image signal, is received in an inside part of a
5 conductive housing which is grounded, so that an electromagnetic wave shielding is attempted and an electromagnetic wave noise leaked to an outside part of the housing is reduced.

However, according to the related art copy
10 machine, it is required to form a space part such as a hole, opening, or gap at the housing in order to radiate heat generated from an electronic apparatus which is received at the conductive housing. Because of this, there is a problem in that it may be
15 difficult to cope with both an effect of radiant heat and a shield against electromagnetic wave noise due to the leakage of the electromagnetic wave noise from the space part.

Particularly, in the related art copy
20 machine, a reading apparatus of an operations clock having a high frequency and a signal processing part are provided at the housing to form a scanner of the image read part. Hence, according the related art copy machine, even if the electronic apparatus is
25 received at the conductive housing, it may be

possible that the electromagnetic wave noise leaks out from a small space part for radiating heat.

SUMMARY OF THE INVENTION

5 Accordingly, it is a general object of the present invention to provide a novel and useful method for reducing electromagnetic disturbance waves and a housing structure, in which one or more of the problems described above are eliminated.

10 Another and more specific object of the present invention is to provide a method for reducing electromagnetic disturbance waves and a housing structure, so that it is possible to cope with both an effect of radiant heat and a shield against the
15 electromagnetic wave noise without making the structure of an electronic apparatus complex. This includes consideration of a positioning relationship between an electromagnetic field of a resonance frequency determined by a measurement of a housing
20 where the electronic apparatus is installed, and a distribution of an electric current sent on a surface of the housing, and a space part of the housing.

 Another object of the present invention is to provide a method for reducing electromagnetic
25 disturbance waves and a housing structure, so that it

is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise by using a housing which can be easily manufactured.

5 The above objects of the present invention are achieved by a method for reducing an electromagnetic disturbance wave generated at an electronic apparatus, by covering the electronic apparatus with a housing which is formed by a
10 material having a shield effect against an electromagnetic wave, including:

 providing a space forming part for radiation of heat or wiring at the housing, so that a longitudinal direction of the space forming part is
15 along a surface electric current distribution in a case where the space forming part is not provided at the housing.

 The above objects of the present invention are achieved by a housing structure for reducing an
20 electromagnetic disturbance wave generated at an electronic apparatus, by covering the electronic apparatus with a housing which is formed by a material having a shield effect against an electromagnetic wave; including:

a space forming part for radiation of heat or wiring at the housing,

wherein a longitudinal direction of the space forming part is along a surface electric
5 current distribution in a case where the space forming part is not provided at the housing.

According to the above mentioned inventions, it is possible to cope with both an effect of radiant heat and high shield-ability against the
10 electromagnetic wave noise under a simple structure.

In the method or housing structure, the housing may be formed by a material including a conductor or a semiconductor which has a volume resistivity of less than or equal to 10^4 „cm.

15 According to the above mentioned invention, even if the housing is not formed by a metal, it is possible to accomplish the shield effect.

In the method or housing structure, the space forming part may be formed so as to have a slit
20 shape or a rectangular shape, and the space forming part in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current of the housing.

According to the above mentioned invention,
25 it is possible to cope with both an effect of radiant

heat and high shield-ability against the electromagnetic wave noise under a more simple structure.

In the method or housing structure, the
5 housing may have a rectangular parallelepiped shape, and the space forming part in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current calculated by a designated numerical formula.

10 According to the above mentioned invention, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure, and to position the space properly under a
15 calculation of the surface electric current distribution with a numerical analysis for example, even if the housing does not have the a rectangular parallelepiped shape.

In the method or housing structure, the
20 space forming part may be formed so as to have a slit shape or a rectangular shape, and the space forming part in the longitudinal direction may be formed radially from a center part of a magnetic field situated at an inside part of the housing, calculated
25 by a designated numerical formula.

According to the above mentioned invention,
it is possible to cope with both an effect of radiant
heat and high shield-ability against the
electromagnetic wave noise under a simple structure,
5 and to position the space part properly under a
calculation of a center position of the magnetic
field with a numerical analysis, for example, even if
the housing does not have a rectangular
parallelepiped shape.

10 In the method or housing structure, a
measurement of the housing may be set so that a
resonance frequency of an electromagnetic wave in the
housing is generated only by a frequency higher than
an upper limit frequency of EMI (Electro Magnetic
15 Interference).

According to the above mentioned invention,
it is possible to make the strength of the
electromagnetic field that is leaked constant.

In the method or housing structure, a hole
20 forming part other than the space forming part may be
provided, and a size of the hole forming part may be
set so as to be less than or equal to one fourth,
more preferably less than or equal to one tenth, of
the wavelength of an electromagnetic wave to be
25 reduced.

According to the above mentioned invention,
it is possible to cope with both an effect of radiant
heat and high shield-ability against the
electromagnetic wave noise under a simple structure,
5 and to estimate, in advance, a shield effect in a
case where the hole is formed at the housing.

In the method or housing structure, the
space forming part may be provided at an upper or
lower part, or the upper and lower parts of the
10 housing.

According to the above mentioned invention,
it is possible to cope with both an effect of radiant
heat and high shield-ability against the
electromagnetic wave noise under a simple structure,
15 and make heat radiative ability higher.

In the method or housing structure, the
housing may have a connection part, and the
connection part in the longitudinal direction may be
provided so as to be along the longitudinal direction
20 of the space forming part.

According to the above mentioned invention,
it is possible to achieve a stable effect of
reduction of electromagnetic wave noise even if the
housing has the connection part, and to cope with
25 both an effect of radiant heat and high shield-

ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, the housing may have a connection part, and the
5 longitudinal direction of the connection part may be along a surface electric current distribution in a case where the connection part is not provided at the housing.

According to the above mentioned invention,
10 it is possible to achieve a stable effect of reduction of electromagnetic wave noise even if the housing has the connection part, and to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under
15 a simple structure.

In the method or housing structure, the connection part in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current of the housing.

20 According to the above mentioned invention, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, since the connection part in the
25 longitudinal direction is arranged in a most proper

direction, even if the housing does not have a rectangular parallelepiped shape, it is possible to position the connection part properly under a calculation of the surface electric current distribution with a numerical analysis, for example, so that higher shield-ability can be achieved.

In the method or housing structure, the housing may have a rectangular parallelepiped shape, and the connection part in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current calculated by a designated numerical formula.

According to the above mentioned invention, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, since the housing has a rectangular parallelepiped shape, it is possible to arrange the connection part properly under a simple calculation of the surface electric current distribution with a numerical analysis, for example, so that higher shield-ability can be achieved.

In the method or housing structure, the housing may have a connection part having a good electrical resistance and a connection part having a

bad electrical resistance, and the connection part having the bad electrical resistance in a longitudinal direction may be along a surface electric current distribution in a case where the
5 connection part having the bad electrical resistance is not provided at the housing.

According to the above mentioned invention, it is possible to stably effect reduction of electromagnetic wave noise even if the housing has
10 the connection part having bad conductivity, and to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, it is possible to provide a housing which can be
15 manufactured easily by arranging the connection part having bad conductivity so as not to disturb the surface electricity current.

In the method or housing structure, the connection part having the bad electrical resistance
20 in a longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current of the housing.

According to the above mentioned invention, it is possible to cope with both an effect of radiant
25 heat and high shield-ability against the

electromagnetic wave noise under a simple structure.
Furthermore, since the connection part having bad
electric resistance in the longitudinal direction is
arranged in a most proper direction, even if the
5 housing does not have a rectangular parallelepiped
shape, it is possible to position the connection part
having bad electric resistance properly under a
calculation of the surface electric current
distribution with a numerical analysis, for example,
10 so that a higher shield-ability can be achieved.

In the method of housing structure, the
housing may have a rectangular parallelepiped shape,
and the connection part having the bad electrical
resistance in the longitudinal direction may be
15 formed radially from a gush part or a concentration
part of the surface electric current calculated by a
designated numerical formula.

According to the above mentioned invention,
it is possible to cope with both an effect of radiant
20 heat and high shield-ability against the
electromagnetic wave noise under a simple structure.
Furthermore, since the housing has a rectangular
parallelepiped shape, it is possible to arrange the
connection part having a bad electric resistance
25 properly under a simple calculation of the surface

electric current distribution with a numerical analysis for example, so that higher shield-ability can be achieved.

In the method or housing structure, the
5 space forming part may be arranged in a direction in which a flow of a cooling medium for elimination of heat or air change is not disturbed.

According to the above mentioned invention,
it is possible to cope with both an effect of radiant
10 heat and high shield-ability against the electromagnetic wave noise under a simple structure, and to obtain a higher radiant heat transfer effect.

In the method or housing structure, a pipe for communicating between an inside and an outside of
15 the housing may be provided at the housing, and a width of an opening part of the pipe may be set so as to be less than or equal to a half of a wavelength of a frequency to be reduced.

According to the above mentioned invention,
20 the electromagnetic wave having a frequency which is lower than a frequency to be reduced to cannot be leaked from a pipe through which a signal line which connects the inside and the outside of the housing passes, and therefore it is possible to keep high
25 shield-ability against the electromagnetic wave noise.

In the method or housing structure, a harness or an electrical wire or cord for communicating information or electric power between the electric apparatus situated at the inside of the housing and an outside of the housing, may be provided at the housing, so as to not disturb a surface electrical current distribution in a case where the harness or the electrical wire or cord is not provided at the housing.

According to the above mentioned invention, in a case where the harness or the electrical wire or cord is provided at the housing, good shield-ability against the electromagnetic wave noise can be obtained. Accordingly, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, an electric optical conversion element for converting an electric signal of the electric apparatus provided at an inside of the housing to an optical signal, an optical fiber for sending the optical signal converted by the electric optical conversion element from the space forming part to an outside of the housing, and an optical electric conversion element

for converting the optical signal which is sent to the outside of the housing by the optical fiber to an electric signal, may be provided,

so that the electric signal of the electric
5 apparatus in the housing is converted to the optical signal by the electric optical conversion element, the converted optical signal is sent from the space forming part to the optical electrical conversion element at the outside part of the housing and is
10 converted to the electric signal, and

therefore information is communicated between the electric apparatus situated at the inside of the housing and the outside of the housing.

According to the above mentioned invention,
15 it is possible to optically communicate a signal between the electronic apparatus situated at the inside of the housing and the outside of the housing. Therefore, it is possible to avoid leakage of an electromagnetic wave from an opening part for signal
20 transmission at all frequencies. Hence, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, an
25 electric infrared conversion element for converting

an electric signal of the electric apparatus provided
at an inside of the housing to an infrared signal,
and an infrared electric conversion element for
converting the infrared signal which is converted by
5 the electric infrared conversion element to an
electric signal, may be provided,

so that the electric signal of the electric
apparatus in the housing is converted to the infrared
signal by the electric infrared conversion element,
10 the converted infrared signal is sent from the space
forming part to the outside part of the housing, and
the infrared signal sent to the outside part of the
housing is converted to the electric signal by the
infrared electric conversion element, and

15 therefore information is communicated
between the electric apparatus situated at the inside
of the housing and the outside of the housing.

According to the above mentioned invention,
it is possible to communicate a signal between the
20 electronic apparatus situated at the inside of the
housing and the outside of the housing by infrared.
Therefore, it is possible to avoid leakage of an
electromagnetic wave from an opening part for signal
transmission at all frequencies. Hence, it is
25 possible to cope with both an effect of radiant heat

and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, it is possible to build a system at a low cost.

5 In the method or housing structure, a heat pipe for radiating heat generated at the electric apparatus provided at the inside of the housing to an outside part of the housing, may be provided along a wall surface of the housing.

10 According to the above mentioned invention, it is possible to raise the heat radiative ability and to avoid reduction of the shield-ability against the electromagnetic wave due to disturbance of an original surface electricity current and magnetic field distribution. Therefore, it is possible to
15 achieve an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, the housing may be formed by a metal material.

20 According to the above mentioned invention, it is possible to further achieve an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, the
25 housing may have an internal surface or external

surface where a thin film formed by a conductor is applied..

According to the above mentioned invention,
it is possible to achieve the same result as the
5 metal housing by a plastic which can be easily
manufactured.

In the method or housing structure, the
housing may be formed by a material having a volume
resistivity of greater than or equal to 10^8 „cm, and
10 the housing may have an internal surface or external
surface where a thin film formed by a material having
a volume resistivity of less than or equal to 10^{-4} „cm
is applied.

According to the above mentioned invention,
15 it is possible to form a housing having a shield
effect by using various kinds of materials.

In the method or housing structure, the
housing may be formed by a plastic material, and the
housing may have an internal surface or external
20 surface where a metal thin film is applied.

According to the above mentioned invention,
it is possible to form the housing having the same
shield effect as the metal housing by a plastic which
can be easily manufactured. Hence, it is possible to
25 cope with both an effect of radiant heat and high

shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, a thickness of the thin film may be greater than a skin
5 depth of a skin effect at a lower limit frequency under an EMI (ElectroMagnetic Interference) regulation.

According to the above mentioned invention, it is possible to cope with both an effect of radiant
10 heat and high shield-ability against the electromagnetic wave noise under a simple structure. In addition, since the thickness of the thin film layer can be estimated in advance, it is possible to obtain an effective shield effect.

15 In the method or housing structure, the thin film layer may be glued to the housing via an adhesion layer, and a sticking part of the thin film, for gluing the thin film layer, may be provided in a direction along a surface electric current
20 distribution of the housing in a case where the sticking part is not provided.

According to the above mentioned invention, it is possible to use a metal tape which is cheap, for example, as the thin film layer. Hence, it is
25 possible to cope with both an effect of radiant heat

and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, the sticking part of the thin film layer in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current of the housing.

According to the above mentioned invention, it is possible to properly arrange a position where the metal tape is put with a numerical analysis, for example, even if a cheap metal tape is used as the thin film layer. Hence, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure.

In the method or housing structure, the housing may have a rectangular parallelepiped shape, and the sticking part for the thin film layer in the longitudinal direction may be formed radially from a gush part or a concentration part of the surface electric current calculated by a designated numerical formula.

According to the above mentioned invention, it is possible to properly arrange a position where the metal tape is put, using a simple calculation

corresponding to the rectangular parallelepiped shape,
even if a cheap metal tape is used as the thin film
layer. Hence, it is possible to cope with both an
effect of radiant heat and high shield-ability
5 against the electromagnetic wave noise under a simple
structure.

In the method or housing structure, a metal
pipe for communicating between an inside and an
outside of the housing may be provided at the housing
10 so as to come in contact with the thin film layer.

According to the above mentioned invention,
it is possible to prevent the electromagnetic wave
from leaking from the metal pipe provided at the
housing formed by the metal thin layer, and therefore
15 it is possible to keep high shield-ability against
the electromagnetic wave noise.

Other objects, features, and advantages of
the present invention will become more apparent from
the following detailed description when read in
20 conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a perspective view for showing a
structural example of a housing of the present
25 invention; more specifically FIG. 1-(a) is a view for

showing a three dimensional structure of the housing,
and FIG. 1-(b) is a view of a distribution of a
magnetic field generated at the housing, seen from a
Z axis;

5 FIG. 2 is a view of distributions of the
magnetic field and an induced electric current
generated at the housing, seen from a Z axis;

 FIG. 3 is a perspective view showing a
configuration example wherein a lid is not formed at
10 an upper part of the housing;

 FIG. 4 is a perspective view showing a
configuration example wherein an induced electric
current, generated so as to be perpendicular to a
revolving magnetic field distribution, is disturbed;

15 FIG. 5 is a plan view for explaining a
measurement configuration of the housing shown in FIG.
1;

 FIG. 6 is a plan view for explaining a
measurement configuration of a housing shown in FIG.
20 3;

 FIG. 7 is a plan view for explaining a
measurement configuration of a housing shown in FIG.
4;

 FIG. 8 contains graphs showing a frequency
25 characteristic of radiation electrical field strength

in a case where a metal housing is used as the housings shown in FIG. 1 and FIG. 3, more particularly; FIG. 8-(a) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 3 GHz, and FIG. 8-(b) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 1.4 GHz;

FIG. 9 contains graphs showing a frequency characteristic of radiation electrical field strength in a case where a metal housing is used as the housings shown in FIG. 1 and FIG. 4, more particularly; FIG. 9-(a) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 3 GHz, and FIG. 9-(b) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 1.4 GHz;

FIG. 10 is a perspective view showing a metal housing having been manufactured by way of trial for measuring shield-ability, and a monopole antenna provided at a noise source in the housing;

FIG. 11 contains graphs showing a result measured at an anechoic chamber by using two housings having structures shown in FIG. 1 and FIG. 3 in which

the monopole antenna is provided as shown in FIG. 10;
more particularly, FIG. 11-(a) shows gain in a case
where the monopole antenna has a length of 83 mm and
a range of the frequency is set 200 through 1120 MHz,
5 and FIG. 11-(b) shows gain in a case where the
monopole antenna has a length of 33 mm and a range of
the frequency is set 1200 through 2520 MHz;

FIG. 12 is a view showing an arrangement
example of a surface electric current distribution
10 and a space in a case where the housing has an L-
shaped configuration;

FIG. 13 is a perspective view showing an
example wherein a plurality of space parts is
provided at an upper or upper and lower parts of the
15 housing;

FIG. 14 is contains perspective views
showing an example wherein a housing connection
surface is provided along a longitudinal direction of
the space part of the housing; FIG. 14-(a) is a view
20 showing an embodiment of the present invention, and
FIG. 14-(b) is a view showing a comparison example;

FIG. 15 contains views showing an
arrangement example of the surface electric current
distribution and the connection part, in a case where
25 the housing has the L-shaped configuration;

FIG. 16 is a perspective view showing an arrangement example of connection parts wherein a connection part having bad electric resistance and a connection part having good electric resistance are
5 provided at the housing part;

FIG. 17 is a perspective view showing an example wherein a tube, which connects an inside and an outside of the housing, is provided at the housing;

10 FIG. 18 contains schematic diagrams of an arrangement example wherein a harness or an electrical wire or cord is provided at the housing;

FIG. 19 is a schematic diagram showing an example wherein an electric optical conversion
15 element, an optical electric conversion element, and an optical fiber are provided at the housing;

FIG. 20 is a schematic diagram showing an example wherein an electric infrared conversion element, and an infrared electric conversion element
20 are provided at the housing;

FIG. 21 contains schematic diagram showing an example wherein a heat pipe is provided at the housing; FIG. 21-(a) is a view showing an embodiment of the present invention, and FIG. 21-(b) is a view
25 showing a comparison example;

FIG. 22 is a side view showing an example wherein a metal thin film is applied to the housing;

FIG. 23 contains graphs showing a frequency characteristic of radiation electrical field strength in a case where a plastic housing to which a metal thin film layer is applied is used as the housings shown in FIG. 1 and FIG. 3, more particularly; FIG. 23-(a) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 3 GHz, and FIG. 23-(b) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 1.4 GHz; and

FIG. 24 contains graphs showing a frequency characteristic of radiation electrical field strength in a case where a plastic housing to which a metal thin film layer is applied is used as the housings shown in FIG. 1 and FIG. 4, more particularly; FIG. 24-(a) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 3 GHz, and FIG. 24-(b) shows a frequency characteristic of radiation electrical field strength in a case of a frequency from 0 Hz to 1.4 GHz.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

A description of an image reader apparatus

and a cylinder shaped lamp for the same, is given below, with reference to the FIGS. 1 through 24 of embodiments of the present invention.

(First embodiment)

5 Referring to FIG. 1-(a), an electronic apparatus such as a printed board 2 wherein an electronic circuit (not shown) and a board line 2b are provided, is installed at an inside of a structure body (housing) 1 having a box configuration and formed by a material having a shield effect
10 against an electromagnetic wave. At an upper surface of the housing 1, a plurality of the spaces (space forming parts) 3 for radiant heat transfer which have slit shapes are formed.

15 Thus, it is possible to reduce an electromagnetic disturbance wave generated by the printed board 2 by covering the printed board 2 provided inside of the housing 1 with the housing 1 formed by the material having the shield effect
20 against the electromagnetic wave.

 A resonance frequency f at the housing 1 is calculated by the following formula 1, wherein a length in an X direction of the housing 1 is set as "a"; a length in a Y direction of the housing 1 is
25 set as "b"; a length in a Z direction of the housing

1 is set as "c"; and a velocity of the electromagnetic wave is set as "v".

(Formula 1)

$$f = v \cdot \sqrt{\left(\frac{m}{2a}\right)^2 + \left(\frac{n}{2b}\right)^2 + \left(\frac{q}{2c}\right)^2}$$

$$m = 1, 2, 3, \dots, n = 1, 2, 3, \dots, q = 0, 1, 2, \dots$$

5 In the above formula 1, "m" represents a number of a magnetic patter in an X direction, "n" represents a number of a magnetic patter in a Y direction, and "q" represents a number of a magnetic patter in a Z direction.

10 Next, referring to FIG. 1-(b), a distribution of a magnetic field at some magnetic field pattern is discussed.

 Here, FIG. 1-(b) is a view of a distribution of a magnetic field generated at the housing 1, seen
15 from a Z axis in a case where 3 is input into the "m"; 2 is input into the "n"; and "0" is input into the "q" in the formula 1. In FIG. 1-(b), a reference letter "4" represents a magnetic field distribution which revolves in the housing 1, and reference

letters "C1, 1" through "C3, 2" represent center positions of the magnetic field distribution which revolves in the housing 1.

Furthermore, in FIG. 1-(b), a position of
5 "Cm1, n1 (m1=1 through m wherein "m" is an optional integer, n1=1 through n wherein "n" is an optional integer) is calculated by the following formula 2.
(Formula 2)

$$C_{m1, n1} = (\frac{a}{2m} + \frac{a}{m}(m1 - 1), -(\frac{b}{2n} + \frac{b}{n}(n1 - 1)))$$

10 Here, in the housing 1, in a case of a=200 mm, b=200 mm, and c=50 mm, a lowest resonance frequency has a value of 1.061 GHz wherein "m" equals 1, "n" equals 1, and "q" equals 0.

According to a boundary condition of the
15 housing 1, the magnetic field distribution in the housing 1 is in a tangent direction of a metal surface. One magnetic field distribution which revolves is controlling in the housing even in a case where the frequency has a value less than 1 GHz and
20 is similar with a case of "m" equals 1, "n" equals 1, and "q" equals 0.

FIG. 2 is a view of the view shown in FIG. 1-(b) and seen from a Z axis, in a state where the

frequency has a value less than or equal to 1 GHz.
In FIG. 2, the electronic apparatus (printed board) 2
is installed in the housing 1. A plurality of the
spaces 3 having the slit shapes are formed at the
5 housing 1. The magnetic field distribution 4 in the
housing 1 is one magnetic field distribution which
revolves.

In the formula 2, if 1 is input into "m", 1
is input into "n", 0 is input into "q", 1 is input
10 into "m1", and 1 is input into "n1", a formulation of
"C1, $1=(a/2, -b/2)$ " is obtained. The spaces 3 having
slit shapes are provided radially in a state where a
center position of an upper lid of the housing 1 is
at the center. An induced current 5 (shown as a
15 dotted line in FIG. 2) which is sent on the lid
situated at the upper part of the housing 1 is sent
so as to counter the magnetic field distribution at
an inside part of the housing.

In the present invention, the space 3 is
20 provided so that longitudinal directions of the
spaces 3 having slit shapes are along a surface
electric current distribution of the induced current
5 in a case where the space 3 is not formed in the
housing 1. More specifically, the space 3 having the
25 slit shapes in the longitudinal direction are formed

radially from a gush part or a concentration part of the surface electric current of the housing, namely a center position of the magnetic field in the housing calculated by the above mentioned formula.

5 In a case where the frequency is between 0 and 1 GHz, the magnetic field in the housing which revolves is controlling. An induced current 5 (shown as a dotted line in FIG. 2) which is sent on the lid situated at the upper part of the housing 1 is sent
10 so as to counter the magnetic field distribution at an inside part of the housing. Hence, directions of the magnetic field in the housing are a direction from a center of the lid of the housing 1 to an end part and a direction from the end part to the center
15 part.

 The space 3 having the slit shape which is provided at the housing 1 is provided so as to be perpendicular to a magnetic field distribution vector, namely so as to be along a direction of the induced
20 current 5, from a center part of a revolution of the magnetic field distribution vector. Hence, it is possible to obtain a shield effect of the electromagnetic wave noise in a state where an induced current generated at the lid of the housing 1
25 is not disturbed and the spaces 3 having the slit

shapes are provided at the housing 1 , and therefore it is possible to obtain the radiant heat effect (transfer of radiant heat).

Next, an effect obtained by the housing 1
5 having the above-discussed structure is tested by a numerical simulation. Radiation electrical field strengths of a configuration (CASE 1) radial from a center part as the spaces 3 having the slit shape in FIG. 1, a configuration (CASE 2) having no lid at all
10 at the upper part of the housing as shown in FIG. 3, and a configuration (CASE 3) disturbing the induced current generated so as to be perpendicular to the revolving magnetic field distribution as the spaces 7 having the slit shape in FIG. 4, are calculated.
15 Here, the housing 1 is formed by a metal material, and therefore a volume resistivity of a general metal is used.

Measurement configurations of FIG. 1, FIG. 3 and FIG. 4 are shown in FIG. 5, FIG. 6, and FIG. 7.
20 Here, "a" is 200 mm, "b" is 200 mm, "d" is 85 mm, "e" is 35 mm, "f" is 70 mm, and "g" is 5 mm. Here, an evaluation is implemented by a simulation of a numerical analysis method which is called the Finite Difference Time-Domain method (FDTD method). In this
25 analysis, an analysis space is divided into lattice

parts and the Maxwell equation is put in differential form and calculated with a time domain. More specifically, a Gaussian pulse is input to an input end of the printed board 2 which is an input point and an output wave shape taken at an operation point in the right upper part of the housing is Fourier transformed, so that information in the frequency domain can be obtained.

First, radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE2 (comparison example) shown in FIG. 3 are calculated from an electric field right in the right upper part of the lid of the housing 1. The radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE 2 are shown in FIG. 8.

FIG. 8-(a) shows radiation electrical field strength in a case of a frequency from 0 Hz to $3.00\text{E}+09$ Hz (3 GHz), and FIG. 8-(b) shows a radiation electrical field strength in a case of a frequency from 0 Hz to $1.50\text{E}+09$ Hz (1.5 GHz). In this embodiment, 3.00×10^9 is represented as $3.00\text{E}+09$.

As understood from FIG. 8-(b), in a case of the CASE 2 wherein the lid is opened, the electric field strength wherein the frequency is between $2.00\text{E}+08$ Hz (200 MHz) and $1.00\text{E}+09$ Hz (1 GHz),

exceeds $8.00\text{E}-06$ V/m. On the other hand, in a case of the CASE 1, the electric field strength wherein the frequency is between $2.00\text{E}+08$ Hz (200 MHz) and $1.00\text{E}+09$ Hz (1GHz), is less than or equal to $3.00\text{E}-06$ V/m. Thus, the CASE 3 wherein the spaces have a slit shape radially from the center part of the housing 1 of the CASE 1 has a shield effect twice as or more than twice of the CASE 2 wherein the lid is not provided at the housing, in the case where the frequency ranges between $2.00\text{E}+08$ Hz (200 MHz) and $1.00\text{E}+09$ Hz (1 GHz).

The above mentioned value is a rough value for proving the shield effect by comparing the CASE 1 and CASE 2.

Next, radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE 3 (comparison example) shown in FIG. 4 are calculated from an electric field in the right upper part of the lid of the housing. The radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE 3 are shown in FIG. 9.

FIG. 9-(a) shows radiation electrical field strength in a case of a frequency from 0 Hz to $3.00\text{E}+09$ Hz (3 GHz), and FIG. 9-(b) shows radiation electrical field strength in a case of a frequency

from 0 Hz to 1.50E+09 Hz (1.5 GHz). In this embodiment, 3.00×10^9 is represented as 3.00E+09.

As understood from FIG. 9-(b), in a case of the CASE 3, the electric field strength wherein the frequency is between 2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz), exceeds 6.00E-06 V/m. On the other hand, in a case of the CASE 1, the electric field strength wherein the frequency is between 2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz), is less than or equal to 3.00E-06 V/m. Thus, the CASE 1 has a shield effect twice or more than twice of the CASE 3 in the case where the frequency range between 2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz). As shown in FIG. 9-(b), a leakage electric field of the CASE 1 is substantially constant in the case of the frequency between 0.00E+00 Hz and 1.00E+08 Hz (1GHz). Furthermore, the spaces having a slit shape cause a radiant heat effect.

As clearly shown by data of FIG. 9-(a), even in a case of a frequency higher than 1.061GHz which is a lowest resonance frequency, the leakage electric field of the CASE 1 is lower than the leakage electric field of the CASE 3, and shield-ability against the CASE 1 is higher than shield-ability against the CASE 3.

Next, housings satisfying the above data were manufactured by way of trial and shield-abilities thereof were examined by measurement in an anechoic chamber.

5 A housing (CASE 1), as shown in FIG. 1, wherein a plurality of the spaces 3 having the slit shapes are provided radially from a center part so as to be along an induced electric current distribution at a housing surface, and a housing (CASE 3), as
10 shown in FIG. 4, wherein a plurality of the spaces 3 having the slit shapes are provided so as to disturb the induced current generated along the revolving magnetic field distribution, were applied as housings manufactured by way of trial.

15 The above mentioned housings are formed by alumina. As a noise source, not printed boards but monopole antenna 2b shown in FIG. 10 was used instead of the board line.

 Regarding a position relationship between
20 the monopole antenna 2b and the housing 1, as shown in FIG. 10, "h" is set as 100 mm, and "i" is set as 25 mm. In addition, lengths of the monopole antenna 2b were set as 33 mm and 83 mm because the radiant efficiency of the electromagnetic wave of the
25 monopole antenna is changed by the frequency.

FIG. 11 shows a measurement result of the housing manufactured by way of trial in the anechoic chamber in which there is a 3m length between a subject of measurement and a measurement antenna.

5 FIG. 11-(a) shows gain in a case where the monopole antenna has the length of 83mm and the range of the frequency is set 200 through 1120 MHz. FIG. 11-(b) shows gain in a case where the monopole antenna has the length of 33 mm and the range of the frequency is
10 set 1200 through 2520 MHz.

In FIG. 11-(a) and FIG. 11-(b), a horizontal axis represents a frequency and a vertical axis represents absolute gain. As shown in FIG. 11-(a), the gain in the CASE 3 is approximately 20 dB higher
15 than the CASE 1. It is found by using electric field conversion that the electromagnetic wave in the CASE 3 outputs easily as approximately 100 times the CASE 1.

In a case of 1058 MHz that is a peak
20 frequency of the CASE 3, the gain of the CASE 3 is approximately 30 dB higher than the CASE 1. This means, by using electric field conversion, the electromagnetic wave in the CASE 3 outputs easily as approximately 100 times the CASE 1.

As described above, it is found that a leakage electric field of the CASE 1 is lower than a leakage electric field of the CASE 3, and shield-ability against the CASE 1 is higher than shield-ability against the CASE 3, through the housings actually manufactured by way of trial.

Thus, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise by a simple structure, namely a structure wherein a plurality of the spaces 3 is provided so that longitudinal directions of the spaces 3 are along a surface electric current distribution of the induced current 5 in a case where the spaces 3 are not provided at the housing 1, more specifically, a structure wherein a plurality of the spaces 3 having slit shapes is provided so that longitudinal directions of the spaces 3 are formed radially from a gush part or a concentration part of the surface electric current calculated by an above-discussed numerical formula (namely, a center part of the magnetic field 4 calculated by the above-discussed numerical formula in the housing). Furthermore, in a case where the housing 1 has a rectangular parallelepiped shape as shown in FIG. 1,

it is possible to position the spaces 3 most properly with a simple calculation.

(Second embodiment)

In the second embodiment, the housing 1
5 having a structure shown in FIG. 1 is formed by a material including a conductor or a semiconductor which has a volume resistivity of less than or equal to $10^4 \Omega \text{cm}$. More specifically, the housing 1 is formed of a semiconductor such as silicon or a metal
10 material such as aluminum or iron.

This is because even if the housing 1 is made by the semiconductor material, the surface electric current is generated at the housing by an inducing function based on a magnetic field
15 distribution in the housing, and the shield effect of the electromagnetic wave can be expected.

Furthermore, in a case where the housing 1 is formed by the material including a conductor or a semiconductor which has a volume resistivity of less
20 than or equal to $10^4 \Omega \text{cm}$, the whole of the housing may be formed by theses materials, or only an internal or external surface may be formed by these materials. That is, in a case where the housing 1 is formed by an insulator such as plastic, as described
25 below, a shield effect can be obtained forming a

metal film on only the internal or external surface of the housing 1, or by applying a conductive agent on only the internal or external surface of the housing 1.

5 In a case where the housing 1 is made by the above mentioned material, as described above in the first embodiment, the spaces 3 are provided at the housing so that a surface electric current distribution in a case where the space is not
10 provided at the housing is not changed. That is, longitudinal directions of a plurality of the spaces 3 having slit shapes are along a surface electric current distribution of the induced electric current
15 housing 1, and therefore a sufficient noise shielding effect can be expected. Thus, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise with a simple structure.

20 Furthermore, the measurement of the housing 1 is set so that the resonance frequency of the electromagnetic wave in the housing is generated only with higher frequencies higher than an upper limit frequency of the EMI regulation. As a result of this,
25 high shield-ability can be obtained until the

resonance frequency reaches 1 GHz as shown in the
CASE 1 of FIG. 9-(b). Thus, it is possible to cope
with both an effect of radiant heat and a shield
against the electromagnetic wave noise with a simple
5 structure, and a higher shieldability effect can be
obtained.

(Third embodiment)

In the third embodiment of the present
invention, a hole (hole forming part) other than the
10 above-described space 3 is provided at the housing 1
having a structure shown in FIG. 1. The hole size is
set so as to be less than or equal to one fourth,
more preferably less than or equal to one tenth, of
the length of an electromagnetic wave to be reduced.

15 For example, there is a description of the
size of an opening part at the housing or the like
and a shield effect, at page 99 of "Noise reduction
techniques in electronic systems", Henry W. Ott.
Although a shield effect of 20 dB can be obtained if
20 the opening part has a size of one twentieth of a
electromagnetic wavelength as an ideal, even if the
opening part has a size of one fourth of the
electromagnetic wavelength, a shield effect of 6 dB
can be obtained. Furthermore, if the opening part
25 has a size less than one tenth of the electromagnetic

wavelength, a sufficient shield effect can be obtained. That is, in a case where the hole is set so as to have a size less than or equal to one fourth, more preferably less than or equal to one tenth, of
5 the wavelength of an electromagnetic wave to be reduced, the effect of radiant heat can be obtained while the effect of the shield against the electromagnetic wave noise is improved.

Here, a shield effect, in a case where a
10 hole having a size of one tenth of the wavelength λ , namely $\lambda/10$, is provided at the housing 1, is described.

According to the above-mentioned "Noise reduction techniques in electronic systems", Henry W.
15 Ott, the shield effect is expressed by the following formula 3, wherein a maximum measurement of the hole provided at the housing is "L" and the wavelength is " λ ".

(Formula 3)

20 $S1=20\text{Log}(\lambda/2L)$

Here, for example, a shield effect of 20 dB means that the electric field strength outside of the housing is one tenth of the electric field strength of an inside of the housing.

Thus, a shield effect of a hole having a size of $\lambda/10$ can be expressed in the following formula 4 by setting $L=\lambda/10$.

(Formula 4)

5 $S1=20\text{Log}(10_{\mu}/2_{\mu}) \doteq 14$

Here, the above-mentioned formula 3 can be applied to a case where one hole is provided at the housing. An amount of reduction of the shield effect in a case where a number of "N" holes are provided at the housing is expressed by the following formula 5.

(Formula 5)

$S2=-20\text{Log}\sqrt{N}$

For example, a shield effect wherein five holes having a size of $\mu/10$ are provided at the housing is expressed by the following formula 6.

(Formula 6)

$S1+S2=14-20\text{Log}\sqrt{5}=14-7=7$

This result shows that a sufficient shield effect of 14 dB (namely, the electric field strength outside of the housing is one fifth of the electric field strength inside of the housing) can be obtained if only one hole having a size of $\mu/10$ is provided, while a sufficient shield effect of 7 dB (namely, the electric field strength outside the housing is $1/2.2$ of the electric field strength inside the housing)

can be obtained if the five holes having sizes of $\lambda/10$ are provided. Hence, the more the number of the holes provided at the housing, the lower the shield effect.

5 Thus, in a case where the number of the holes provided at the housing is small such as just only one, a shield effect can be obtained even if the size of the hole is less than one fourth of the wavelength. However, in order to obtain sufficient
10 shield effect, it is preferable that the size of the hole be less than one tenth of the wavelength. In addition, in a case where a plurality of the holes is provided at the housing, a hole is required to have a size less than one tenth of the wavelength. Because
15 of this, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise, and estimate the shield effect in a case where the hole is formed in the structural body in advance.

20 (Fourth embodiment)

 In the fourth embodiment, a space having a slit shape or rectangular shape is provided at the housing, and a longitudinal direction of the space is set so that a surface electric current distribution
25 in a case where the space is not provided at the

housing is not changed. That is, as shown in FIG. 1,
in a case where the spaces 3 having slit shapes are
provided at the housing 1, the longitudinal
directions of a plurality of the space 3 having slit
5 shapes are along a surface electric current
distribution of the induced electric current 5 in a
case where the spaces are not provided at the housing
1.

For example, there is a description about
10 the way to form an opening part at the housing, for
example, at page 198 of "Noise reduction techniques
in electronic systems", Henry W. Ott. It is
discussed that a surface electric current
distribution is disturbed by a slit having a
15 rectangular configuration so that a shield effect is
reduced, in the description.

In this embodiment, a longitudinal direction
of the space having the slit shape or the rectangular
shape is set so that a surface electric current
20 distribution is not disturbed and therefore a high
shield effect can be obtained. Hence, it is possible
to cope with both an effect of radiant heat and a
shield against the electromagnetic wave noise with a
simple structure, and to position the space having a
25 slit shape or rectangular shape most properly.

(Fifth embodiment)

In the fifth embodiment, the space having a slit shape or a rectangular shape in the longitudinal direction is formed radially from a gush part or a concentration part of the surface electric current of the housing.

As shown in FIG. 1, in a case where the housing 1 has a rectangular parallelepiped configuration, a resonance frequency, or a gush part or a concentration part of the surface electric current of the housing part, namely a center part of the magnetic field, can be obtained analytically. Hence, it is possible to position a longitudinal direction of the space 3 so that the space in the longitudinal direction is formed radially from a gush part or a concentration part of the surface electric current of the housing.

However, as shown in FIG. 12-(a), in a case where the housing 1 has an L-shaped configuration, a resonance frequency or a gush part or a concentration part of the surface electric current of the housing part, namely a center part of the magnetic field, cannot be obtained analytically. In this case, a numerical analysis such as the above-described FDTD method is performed or a vicinity magnetic

distribution is calculation-analyzed so that a surface electric current distribution shown by a numerical mark 5 in FIG. 12-(b) is obtained. A longitudinal direction of the space 3 from a position of a gush part or a concentration part of the surface electric current of the housing part is radially set so that a shield effect can be improved. Thus, both an effect of radiant heat and a shield against the electromagnetic wave noise are coped with using a simple structure. In addition, even if the housing does not have a rectangular parallelepiped configuration, the surface electric current distribution can be calculated by a numerical analysis, so that it is possible to position the space most properly.

(Sixth embodiment)

Next, referring to FIG. 13, a sixth embodiment of the present invention wherein a plurality of the space parts is provided at an upper part of the housing or the upper or lower part of the housing is explained.

As shown in FIG. 13, the spaces 3 having slit shapes are provided at an upper part of the housing 1, and a plurality of the spaces 3b having

slit shapes is provided at a bottom surface part of the housing 1.

Thus, since the spaces 3 having slit shapes are provided at the upper part and the bottom surface part of the housing 1, it is possible to achieve more effective radiant heat effect based on a convection current. The space having a slit shape may be provided only at the bottom surface part of the housing 1. Furthermore, in a case where a plurality of the spaces 3 having slit shapes is provided at an upper part of the housing 1, and a plurality of the spaces 3b having slit shapes is provided at a bottom surface part of the housing 1, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise with a simple structure, by forming the spaces 3 and 3b in the longitudinal directions radially from a gush part or a concentration part of the surface electric current of the housing 1.

(Seventh embodiment)

In the seventh embodiment of the present invention, a connection part is provided at the housing so that a surface electric current in a case where the connection part is not provided at the housing is not changed.

Generally the connection part has a higher resistance value than the housing, and thereby the surface electric current is disturbed. Hence, it is possible to achieve a sufficient shield effect by providing the connection part at the housing so that a surface electric current in a case where the connection part is not provided at the housing is not changed. Thus, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise with a simple structure, and a high shield effect can be achieved even if the connection part is provided at the housing.

Here, referring to FIG. 14, a case where a housing connection part (a connection surface) for connecting the housing 1 is provided along a longitudinal direction of the space part 3 formed at the housing 1, is described.

A housing 1, an electronic apparatus (printed board) 2 installed in the housing 1, a plurality of the spaces 3 having slit shapes, a housing connection surface 8, and a generated induced electric current 9 are shown in FIG. 14-(a).

As long as the same housing configuration and frequency are provided to the case shown in FIG. 14-(a), the induced electrical current 9 is sent from

a center of an upper part lid or to a center part only. Since the housing connection surface 8 is provided along the longitudinal direction of the space part 3 of the housing 1, a stable shield effect
5 which is along the electric current is achieved by a simple conductive process.

FIG. 14-(b) shows a comparison example to the case shown in FIG. 14-(a). The housing connection surface 8b is perpendicular to the induced
10 electrical current 9b. If the conductive process to the housing connection surface 8b is incomplete, the induced electric current is not sent sufficiently and thereby the shield-ability cannot be obtained.

Therefore, it is possible to achieve a
15 stable reduction effect of electromagnetic wave noise even if conductivity of the housing connection part is bad, by providing the housing connection surface so as to be along a longitudinal direction of the spaces 3 formed radially.

20 Thus, in this embodiment, a connection part is provided at the housing so that a surface electric current in a case where the connection part is not provided at the housing is not changed.

As described above, a shield effect is
25 reduced due to disturbance of the surface electric

current by a slit having a rectangular shape.
Similarly and generally, a shield effect is reduced
due to disturbance of the surface electric current by
a connection part with a longitudinal direction.

5 Hence, in a case where the connection has a
longitudinal direction, as described above, it is
possible to improve the shield effect by providing
the longitudinal direction of the connection part so
as to not disturb the surface electric current.

10 Hence, it is possible to cope with both an effect of
radiant heat and a shield against the electromagnetic
wave noise, and most proper positioning can be done
even if the connection part has the longitudinal
direction.

15 (Eighth embodiment)

 In the eighth embodiment of the present
invention, the connection part in the longitudinal
direction is formed radially from a gush part or a
concentration part of the surface electric current of
20 the housing.

 In a case where the housing 1 has a
rectangular parallelepiped configuration, a resonance
frequency or a gush part or a concentration part of
the surface electric current of the housing part,

namely a center part of the magnetic field, can be obtained analytically.

However, as shown in FIG. 15-(a), in a case where the housing 1 has an L-shaped configuration, a
5 resonance frequency or a gush part or a concentration part of the surface electric current of the housing part, namely a center part of the magnetic field, cannot be obtained analytically. In this case, a numerical analysis such as the above-described FDTD
10 method is performed or a vicinity magnetic distribution is calculation-analyzed so that a surface electric current distribution shown by a numerical mark 5 in FIG. 15-(b) is obtained. A longitudinal direction of the housing connection part
15 8 from a position of a gush part or a concentration part of the surface electric current of the housing part is radially set so that a shield effect can be improved. Thus, an effect of radiant heat and a shield against the electromagnetic wave noise can be
20 coped with using a simple structure. In addition, even if the housing does not have a rectangular parallelepiped configuration, the surface electric current distribution can be calculated by a numerical analysis, so that it is possible to position the
25 connection part 8 most properly.

In a case where the housing 1 has a rectangular parallelepiped configuration, a resonance frequency or a gush part or a concentration part of the surface electric current of the housing part, namely a center part of the magnetic field, can be obtained analytically. It is possible improve a shield effect by arranging the connection part 8 radially from the gush part or concentration part of the surface electric current as well as a case shown in FIG. 14-(a). Hence, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise, and to position the connection part with a simple calculation most properly in a case where the housing has a rectangular parallelepiped configuration.

(Ninth embodiment)

The ninth embodiment of the present invention is discussed with reference to FIG. 16. A housing 1, a plurality of spaces 3 having slit shapes provided at an upper part of the housing 1, a surface electric current 5 generated at the upper part of the housing 1, a connection part 8 having bad electric resistance (which has a large contact resistance, an unevenness resistance depending on a connection position, and bad conductivity) and a connection part

8 having good electric resistance (which has a small contact resistance, a small unevenness resistance depending on a connection position, and good conductivity) are shown in FIG. 16. In a case where the housing 1 in which an electronic apparatus is installed is manufactured, it is difficult to actually manufacture only one connection part such as the connection part 8 and therefore it causes increasing of cost. Hence, at the time of manufacturing, the upper part of the housing 1 is made to have a lid shape. The upper part lid can be removed so that the connection part is provided at a position by which the numerical mark 8a is indicated in FIG. 16. However, if a housing main body and the upper part lid are connected mechanically such as by using screw-fixing, the contact resistance at the connection part 8a is made large and unevenness of the resistance occurs depending on the contacting position so that an induced electric current generated at the upper part lid may be disturbed. That is, as described in the seventh embodiment, the connection part 8a between the housing main body and the upper part lid faces a direction perpendicular to the induced electric current generated at the upper part lid. Therefore, an electric current is largely

disturbed at the connection part so that the shield effect can be weakened. If the housing main body and the upper part lid are connected by welding or sealing with solder, good conductivity can be

5 obtained and shield-ability can be improved. It is not preferable to apply welding or soldering after the electronic apparatus is installed in the housing because a bad influence due to heat is given to the electronic apparatus. Therefore, it is required to

10 mechanically connect the housing main body and the upper part lid. In this case, a contact resistance at the connection part 8a can be drastically reduced by putting a conductive gasket, for example, at the contact part 8a. Also, it is possible to reduce the

15 resistance unevenness at the contact position by managing the torque of screw fixing, so that a connection part having good electric resistance is obtained. If the connection part 8a at which the conductive gasket is put is opened and closed only at

20 the time of manufacturing, it is possible to maintain a good electric resistance state and provide conductivity. In a case where the housing is opened and closed at the time of maintenance, for example, the connection part 8 having bad electric resistance

25 is used. Because of this, it is possible to improve

a shield effect in which the manufacturing cost is reduced.

As shown in FIG. 16, in a case where the housing 1 has a connection part 8a having good electrical resistance and a connection part 8 having bad electrical resistance, the connection part 8 having bad electrical resistance in a longitudinal direction is along a surface electric current distribution in a case where the connection part 8 having bad electrical resistance is not provided at the housing. More specifically, as described in the seventh embodiment, the connection part 8 having bad electrical resistance in a longitudinal direction is formed radially from a gush part or a concentration part of the surface electric current of the housing. That is, the connection part 8 having bad electrical resistance is positioned as well as the space 3 having a slit shape.

Particularly, in a case where the housing 1 has a rectangular parallelepiped shape, the connection part having the bad electrical resistance in the longitudinal direction is formed radially from a gush part or a concentration part of the surface electric current calculated by the above mentioned numerical formula. Because of this, it is possible

to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, it is possible to provide a housing easily manufactured by
5 arranging a position of the connection part so that the surface electric current distribution is prevented from being disturbed.

(Tenth embodiment)

In the above mentioned embodiments, the
10 space is arranged radially from a gush part or a concentration part of the surface electric current and in a direction which a flow of a cooling medium for elimination of heat or air change is not disturbed. That is, radiant heat by the space 3 and
15 a convection current of inside air are calculated by a numerical analysis and a measurement analysis. Based on a result of them, it is possible to arrange the most proper position. Thus, it is possible to improve the radiant heat effect, while a shield
20 effect is improved. Hence, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise by arranging a position of the space 3 most properly, and to further improve the radiant heat effect

25 (Eleventh embodiment)

Next, a case where a pipe for communicating between the inside and the outside of the housing 1 having a similar structure with the housing shown in FIG. 1 is provided at the housing 1, and the width of an opening part of the pipe is set so as to be less than or equal to a half of the wavelength of a frequency to be reduced, is described with reference to FIG. 17.

A pipe 10 is shown in FIG. 17. A numerical mark 10c shows the width of an opening part 10b of the pipe 10. It is assumed that the height of the opening part 10b of the pipe is larger than the width 10c of the opening part 10b. Generally, the electromagnetic wave does not transfer to a metal rectangular waveguide pipe having a width less than a half wavelength of the magnetic wave. If an upper limit frequency of the EMI regulation is set to have 1 GHz, a half wavelength is set as 0.165 m. If the measurement of the width 10c of the opening part 10b is set as 0.165 m, an electromagnetic wave having a frequency less than 1 GHz does not leak from the opening part 10b, and therefore a signal line of an electronic apparatus such as the printed board can be pulled out.

Therefore, it is possible to prevent the electromagnetic wave having a frequency lower than a frequency to be reduced from leaking from the pipe 10 such as a metal pipe provided at the housing 1 for
5 passing the signal line by setting the size of the width 10C of the opening part 10b of the pipe 10 as a length less than or equal to the half of the wavelength of the frequency to be reduced.

(Twelfth embodiment)

10 Next, the twelfth embodiment is explained with reference to FIG. 18.

In FIG. 18, a housing 1, a printed board 2 which is one example of an electronic apparatus, and a harness 21 (or electrical wire or cord) extending
15 from the printed board 2, are shown. In a case where a harness 21 (or an electrical wire or cord) for communicating information or electric power between the electric apparatus situated at the inside of the housing and the outside of the housing, is provided
20 at the housing, if the harness 21 (or electrical wire or cord) is provided as shown in FIG. 18-(a), based on a boundary condition of the harness 21 (or electrical wire or cord), a magnetic field distribution of the inside of the housing is
25 disturbed so that the surface electric current is

also disturbed. Hence, in this embodiment, the harness 21 (or electrical wire or cord) for communicating information or electric power between the electric apparatus situated at the inside of the housing and the outside of the housing, is provided at the housing 1, so as to not disturb a surface electrical current distribution in a case where the harness (or electrical wire or cord) is not provided at the housing 1. More specifically, as shown in FIG. 18-(b), it is possible to reduce the disturbances of the magnetic field in the housing and the surface electric current by providing the harness 21 (or electrical wire or cord) close to a wall surface of the housing 1, so that a good shield effect can be achieved even if the harness (or electrical wire or cord) is put to the housing. Hence, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise with a simple structure, and to obtain a good shield effect even if the harness (or electrical wire or cord) is put to the housing.

(Thirteenth embodiment)

Referring to FIG. 19, in the thirteenth embodiment, an electric optical conversion element for converting an electric signal to an optical

signal, an optical electric conversion element for
converting the optical signal to an electric signal,
and an optical fiber, are provided at the housing
having a similar structure with a structure shown in
5 FIG. 1.

The electric optical conversion element 11,
the optical fiber 12, and the optical electric
conversion element 13 are provided in FIG. 19. The
electric optical conversion element 11 converts an
10 electric signal of the electric apparatus 2 such as
the printed board to an optical signal. The optical
signal converted by the electric optical conversion
element is sent from the space 3 having the slit
shape to an outside of the housing by the optical
15 fiber 12, and then converted to the electric signal
by the optical electric conversion element 13.
Because of this structure, it is possible to
communicate a signal between the inside and outside
of the housing and to avoid leakage of an
20 electromagnetic wave from an opening part for signal
transmission at all frequencies.

That is, in this embodiment, the electric
optical conversion element is connected to an
electric apparatus installed inside of the housing,
25 an optical fiber connected to the electric optical

conversion element is extended out from the space part formed at the housing, and the optical electric conversion element is connected to the optical fiber. Because of this structure, the electric signal of the electric apparatus is converted to the optical signal by the electric optical conversion element, the converted optical signal is sent from the space to the optical electrical conversion element provided at the outside part of the housing and is converted to the electric signal by the optical electric conversion element. As a result of this, the signal is better communicated between the electric apparatus situated at the inside of the housing and the outside of the housing, and it is possible to avoid a leakage of an electromagnetic wave from an opening part for signal transmission at all frequencies.

(Fourteenth embodiment)

Referring to FIG. 20, in the fourteenth embodiment, an electric infrared conversion element for converting an electric signal to an infrared signal, and an infrared electric conversion element for converting the infrared signal to an electric signal are provided at the housing having a similar structure with a structure shown in FIG. 1.

The electric infrared conversion element 14, a radiated infrared signal 15, and the infrared electric conversion element 16 are provided in FIG. 20. The electric infrared conversion element 14
5 converts an electric signal of the electric apparatus 2 such as the printed board to the infrared signal 15. The infrared signal 15 converted by the electric infrared conversion element 14 is sent from the space 3 having the slit shape to the outside of the housing,
10 and then converted to the electric signal by the infrared electric conversion element 15. Because of this structure, it is possible to communicate a signal between the inside and outside of the housing and to avoid leakage of an electromagnetic wave from
15 an opening part for signal transmission at all frequencies. Furthermore, it is possible to perform the above with a low cost.

That is, in this embodiment, the electric infrared conversion element is connected to an
20 electric apparatus installed inside of the housing, and the infrared signal radiated from the electric infrared conversion element is sent to the infrared electric conversion element provided at the outside of the housing via the space and converted to the
25 electric signal by the optical infrared conversion

element. As a result of this, the signal is communicated between the electric apparatus situated at the inside of the housing and the outside of the housing, and it is possible to avoid leakage of an
5 electromagnetic wave from an opening part for signal transmission at all frequencies.

(Fifteenth embodiment)

Next, referring to FIG. 21, the fifteenth embodiment in which a heat pipe is provided at a
10 housing 1 having the same structure as the structure shown in FIG. 1, is discussed.

A heat pipe 17 and a generated magnetic field 18 are shown in FIG. 21-(a). Heat generated from an electronic apparatus 2 such as a printed
15 board is made to escape to a housing wall surface 19 by a heat pipe 17. In this case, the heat pipe 17 is provided so as to be along the housing wall surface 19 as close as possible. Generally, a surface of the heat pipe is made by metal, and therefore a magnetic
20 field is distributed in a state where a metal surface is in a tangent direction. However, since the heat pipe 17 is provided so as to be along the housing wall surface 19, the magnetic field distribution 18 is almost not disturbed. Thus, further radiant heat
25 effect can be obtained, and the magnetic field

distribution is not disturbed and thereby a reduction of the shield effect due to the heat pipe does not happen. FIG. 21-(b) is a comparison example of FIG. 21-(a). In FIG. 21-(b), a heat pipe 17b is not
5 provided along with the housing wall surface 19 but provided across a center of the housing. Hence, the magnetic field distribution 18b is disturbed a lot.

Therefore, the radiant heat effect is improved and a disturbance of the magnetic field by
10 the heat pipe and a reduction of shield-ability from the electromagnetic wave can be prevented by providing a heat pipe for connecting an electronic apparatus provided in the housing, along the housing wall surface.

15 (Sixteenth embodiment)

In the sixteenth embodiment, the housing 1 of the first through fifteenth embodiments is formed by a metal. The surface electric current is sent well and a high shield effect can be achieved by
20 forming the housing 1 with the metal. Hence, it is possible to cope with both an effect of radiant heat and a shield against the electromagnetic wave noise, and a high shield effect can be achieved.

(Seventeenth embodiment)

In the seventeenth embodiment, the housing 1 of the first through fifteenth embodiments, the housing has an internal surface or external surface where a thin film formed by a conductor is applied.

5 That is, even if a main material by which the housing 1 is formed is an insulator, shield-ability against the electromagnetic wave noise can be obtained by applying the thin film formed by the conductor to the internal surface or external surface of the housing 1.

10 More specifically, the housing is formed by a material having a volume resistivity of more than or equal to $10^8 \Omega \text{cm}$, and the housing has an internal surface or external surface where a thin film formed by a material having a volume resistivity of less
15 than or equal to $10^{-4} \Omega \text{cm}$ is applied. As the material having a volume resistivity of more than or equal to $10^8 \Omega \text{cm}$, a plastic material can be used. Also, as the material having a volume resistivity of less than or equal to $10^{-4} \Omega \text{cm}$, metal can be used.

20 Because of the above-described structure of the housing, the housing can be formed by plastic which can be easily manufactured. Also, a shield effect of the electromagnetic wave noise and the radiant heat effect that are similar to the effects

obtained by the metal housing of the fifteenth embodiment can be obtained.

Next, an actual effect, in a case where a plastic housing having an inside on which a metal
5 thin film is applied, is examined by simulation.

As shown in FIG. 22 which is a cross-sectional view of the plastic housing 1a, a metal thin film layer 1b is applied to an internal surface side of the plastic housing 1a. A printed board 2 is
10 installed in an inside part of the plastic housing 1a. The housing of this embodiment has a similar structure with the structure of the housing 1 of the first embodiment.

Radiation electrical field strengths of a
15 configuration (CASE 1) with the spaces 3 having the slit shape formed radially from a center part as in FIG. 1, a configuration (CASE 2) having no lid at all at the upper part of the housing as shown in FIG. 3, and a configuration (CASE 3) disturbing the induced
20 current generated so as to be perpendicular to the revolving magnetic field distribution as the space 7 having the slit shape in FIG. 4, are calculated. Measurement configurations of FIG. 1, FIG. 3 and FIG. 4 are shown in FIG. 5, FIG. 6, and FIG. 7. Here, "a"
25 is 200 mm, "b" is 200 mm, "d" is 85 mm, "e" is 35 mm,

"f" is 70 mm, and "g" is 5 mm. The dielectric constant of the plastic is 3 and the plastic has a thickness of 5 mm.

Here, like the first embodiment, an
5 evaluation is implemented by a simulation of a numerical analysis method which is called the Finite Difference Time-Domain method (FDTD method).

First, radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE 2 (comparison
10 example) shown in FIG. 3 are calculated from an electric field in the right upper part of the lid of the housing. The radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE2 are shown in FIG. 23. FIG. 23-(a) shows radiation
15 electrical field strength in a case of a frequency from 0 Hz to 3.00E+09 Hz (3 GHz), and FIG. 23-(b) shows a radiation electrical field strength in a case of a frequency from 0 Hz to 1.40E+09 Hz (1.4 GHz).

As understood from FIG. 23-(b), in a case of
20 the CASE 2 wherein the lid is opened, the electric field strength wherein the frequency is between 2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz), exceeds 1.00E-05 V/m. On the other hand, in a case of the CASE 1, the electric field strength wherein
25 the frequency is between 2.00E+08 Hz (200 MHz) and

1.00E+09 Hz (1 GHz), is less than or equal to 4.00E-06 V/m. Thus, the CASE 3 wherein the spaces have a slit shape radially from the center part of the housing 1 of the CASE 1 has a shield effect twice or
5 more than twice of the CASE 2 wherein the lid is not provided at the housing, in the case where the frequency ranges between 2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz).

Next, radiation electrical field strengths
10 of CASE 1 shown in FIG. 1 and CASE3 (comparison example) shown in FIG. 4 are calculated from an electric field in the right upper part of the lid of the housing. The radiation electrical field strengths of CASE 1 shown in FIG. 1 and CASE 3 are
15 shown in FIG. 24. FIG. 24-(a) shows radiation electrical field strength in a case of a frequency from 0 Hz to 3.00E+09 Hz (3 GHz), and FIG. 24-(b) shows radiation electrical field strength in a case of a frequency from 0 Hz to 1.40E+09 Hz (1.4 GHz).

20 As understood from FIG. 24-(b), in a case of the CASE 3, the electric field strength wherein the frequency is between 5.00E+08 Hz (500 MHz) and 1.00E+09 Hz (1 GHz), exceeds 8.00E-06 V/m. On the other hand, in a case of the CASE 1, the electric
25 field strength wherein the frequency is between

2.00E+08 Hz (200 MHz) and 1.00E+09 Hz (1 GHz), is
less than or equal to 4.00E-06 V/m. Thus, the CASE 1
has a shield effect twice or more than twice of the
CASE 3 in the case where the frequency ranges between
5 5.00E+08 Hz (500 MHz) and 1.00E+09 Hz (1 GHz). As
shown in FIG. 24-(b), a leakage electric field of the
CASE 1 is substantially constant in the case of the
frequency between 0.00E+00 Hz and 1.00E+08 Hz (1 GHz).
Furthermore, the space having a slit shape causes a
10 radiant heat effect.

As clearly shown by data of FIG. 24-(a),
even in a case of a frequency higher than 1.061 GHz
which is a lowest resonance frequency, a leakage
electric field of the CASE 1 is lower than a leakage
15 electric field of the CASE 3, and shield-ability
against the CASE 1 is higher than shield-ability
against the CASE 3.

(Eighteenth embodiment)

In the eighteenth embodiment, a thickness of
20 the thin film of the seventeenth embodiment is
greater than a skin depth of a skin effect at a lower
limit frequency under an electromagnetic interference
(EMI) regulation. More particularly, the surface
electric current is sent to the metal thin film layer
25 smoothly and therefore a high shield effect can be

achieved by making the thickness of the metal thin film layer greater than or equal to several tens of μm . Because of this, it is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. In addition, since the thickness of the thin film payer can be estimated in advance, it is possible to obtain an effective shield effect. (Nineteenth embodiment)

10 In the nineteenth embodiment, the thin film layer in the seventeenth and eighteenth embodiments is glued to the housing via an adhesion layer, and a sticking part of the thin film, for gluing the thin film layer, is provided in a direction along a
15 surface electric current distribution of the housing in a case where the sticking part is not provided. Because of this, it is possible to easily form a metal thin film layer by gluing the metal tape to the inside part of the plastic housing. Hence it is
20 possible to obtain a high shield effect while manufacturing is done easily. It is possible to use a metal tape which is cheap, for example, as the thin film layer. Hence, it is possible to cope with both an effect of radiant heat and high shield-ability

against the electromagnetic wave noise under a simple structure.

(Twentieth embodiment)

In the twentieth embodiment, the sticking
5 part of the thin film layer of the nineteenth
embodiment in the longitudinal direction is formed
radially from a gush part or a concentration part of
the surface electric current of the housing. Because
of this arrangement, it is possible to easily form a
10 metal thin film layer by gluing the metal tape to the
inside part of the plastic housing. Hence it is
possible to obtain a high shield effect while
manufacturing is done easily. It is possible to
properly arrange a position where the metal tape is
15 put with a numerical analysis for example, even in a
case where a metal tape is used as the thin film
layer. Hence, it is possible to cope with both an
effect of radiant heat and high shield-ability
against the electromagnetic wave noise under a simple
20 structure.

(Twenty first embodiment)

The housing in the 21st embodiment has a
rectangular parallelepiped shape, and the sticking
part for the thin film layer in the longitudinal
25 direction is formed radially from a gush part or a

concentration part of the surface electric current calculated by a designated numerical formula.

Because of this arrangement, it is possible to easily form a metal thin film layer by gluing the metal tape to the inside part of the plastic housing. Hence it is possible to obtain a high shield effect while manufacturing is done easily. It is possible to cope with both an effect of radiant heat and high shield-ability against the electromagnetic wave noise under a simple structure. Furthermore, it is possible to properly arrange a position where the metal tape is put under a simple calculation, in a case where the housing has a rectangular parallelepiped configuration.

(Twenty second embodiment)

In the 22nd embodiment, a metal pipe for communicating between the inside and the outside of the housing of the seventeenth through 21st embodiments is provided at the housing so as to come in contact with the thin film layer. In this case, the pipe has a width less than or equal to half of the wavelength of the frequency to be reduced. Because of this structure, the housing having the metal thin film has a substantially same effect as the housing of the eleventh embodiment.

The present invention is not limited to these embodiments, but variations and modifications may be made without departing from the scope of the present invention.

5 For example, although the plastic housing having the inside part where the metal thin film is applied is discussed in the seventeenth through 21st embodiments, the present invention is not limited to these embodiments. A material such as ceramic, glass,
10 wood may be used for the housing so that the housing has an inside part where the metal thin film is applied.

 This patent application is based on Japanese Priority Patent Applications No. 2003-31395 filed on
15 February 7, 2003 and No. 2003-198549 filed on July 17, 2003, the entire contents of which are hereby incorporated by reference.

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